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A METHOD FOR REDUCING DATA FROM
RADIOGRAPHS OF SHAPED-CHARGE JETS

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US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) (hib) This report is a users' guide intended for those involved in reducing data from radiographs of shaped-charge jets. The procedure for setting-up and reading radiographs is listed step-by-step. A computer code listing and description of the calculations are included. Jet particle velocities, break-up time, kinetic energies, lengths, diameters, length-to-diameter ratios, masses, momentums, and jet virtual origin are all included in the code.		

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A

I. INTRODUCTION

With measurements taken directly from flash radiographs of shaped-charge jets before and after breakup, quantitative information describing particulated jet characteristics can be derived. The measurements are used to calculate such properties as particle length, diameter, velocity, mass and break-up time. It is, however, a very tedious and time consuming operation to take the measurements by hand and subsequently perform the calculations at one's desk. To alleviate much of this work, a method using digitizing equipment and a computer program has been developed and is the subject of this report. This method has proven to be very useful, especially in projects involving many rounds and requiring short turn-around time for measurements and computations.^{1,2} The equations used in the computations will be discussed in the next section. Appendices for film reading procedures and for the computer program operation are included.

II. COMPUTATIONS AND EQUATIONS

The program was designed to calculate as many quantities as possible with the data extracted from radiographs. This includes individual particles as well as the whole jet measurements. Since this report is intended as a user's guide, the calculations will be described briefly. All computations are tabulated in the output with proper headings. A typical output is shown in Appendix E.

All radiographs contain slightly magnified images of the particles of a shaped-charge jet. The positions of the particles are likewise altered from their true positions relative to the base of the shaped-charge liner. This difference is taken into account by the magnification factor, M, which is determined by the ratio of the distance, a, from the face of the x-ray tube to the jet path, to the distance, b, from the tube face to the film, as depicted in Figure 1. Thus, $M = a/b$. This factor is used in determining particle lengths, diameters, and positions. To calculate lengths and diameters, the measurements taken from the particle images on film are simply multiplied by the magnification factor.

To calculate change in position the magnification factor is used in the determination of a particle's true position during a given flash. Two cases must be considered regarding the film location in

¹R. L. Jameson, and H. J. Blische, "A Study of a Light Anti-tank Weapon," report in preparation.

²D. Dorfman, and S. K. Golaski, "Electro Formed Shaped Charge Liner Evaluation," report in preparation. Martin Marietta Corp.
Contract #DAAK 11-77-0088.

the determination of position. Refer to Figure 1 for the locations of the terms involved. Note that on all films the distance, p , from the fiducial to the particle is positive below the fiducial and negative above.

Case I: Film numbers 1 and 2.

$$s = F - [(f-p) M] ,$$

where s is the true position, F is the distance from the shaped-charge liner base to the x-ray tube focal level, f is the location of the y fiducial relative to the focal level, p is the point on the particle measured from f , and M is the magnification factor.

Case II: Film numbers 3 and 4

$$s = F + [(f+p) M] .$$

Once the positions have been determined for all flashes, velocity is calculated by

$$v = \frac{s_b - s_a}{T_b - T_a} ,$$

where $s_b - s_a$ is the distance of jet travel between the earlier (a) and later (b) flashes, and $T_b - T_a$ is the change in time between the flashes.

Break-up time is determined by the equation developed by Simon.³

$$t_b = \frac{\sum_{i=1}^n l_i}{v_1 - v_n}$$

where l_i is the individual particle length, v_1 is the velocity of the first particle and v_n is the velocity of the nth particle.

³J. Simon, "The Effect of Explosive Detonation Characteristics on Shaped Charge Performance," BRL Memorandum Report 2414 (1974). (AD #B000337L).

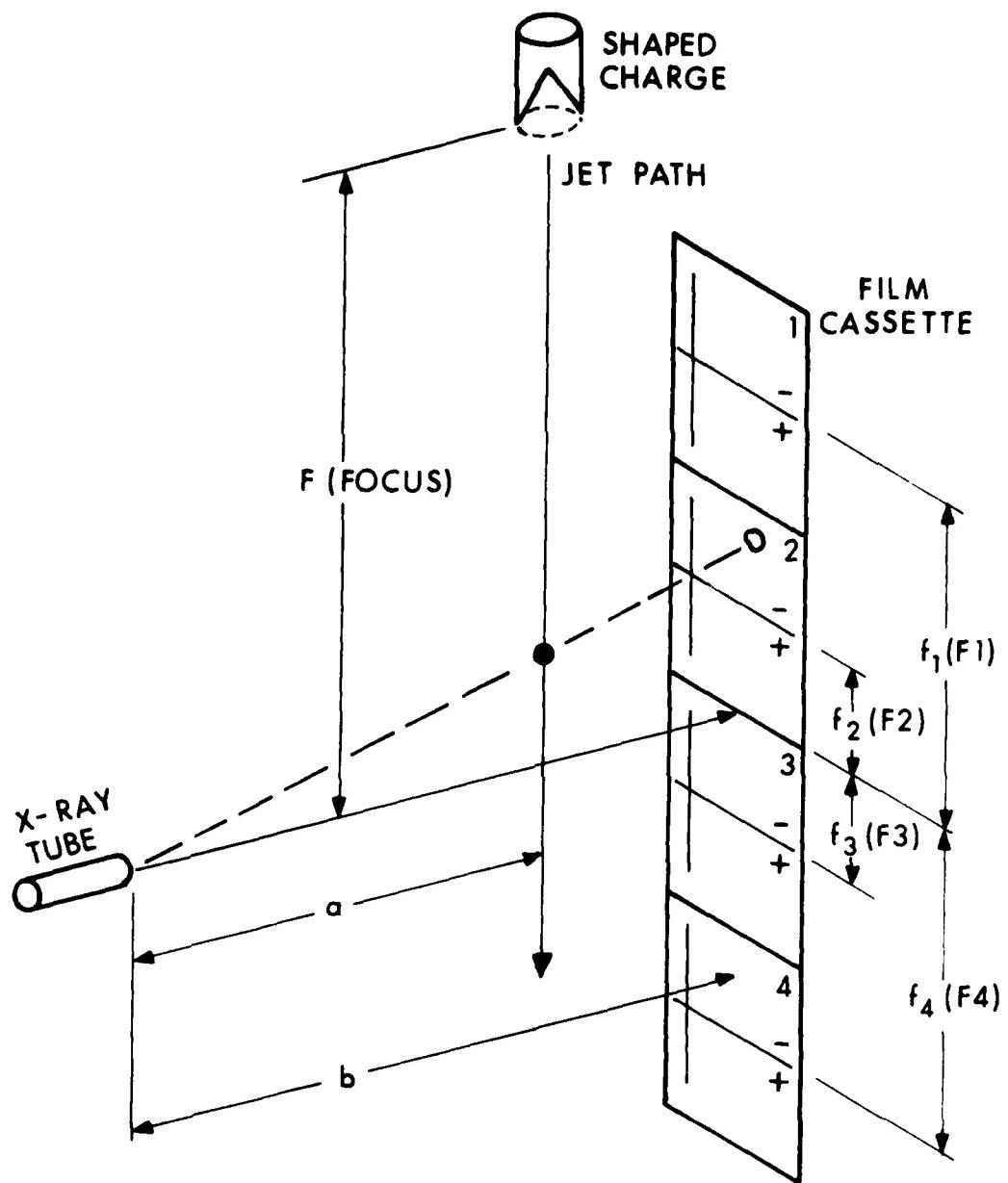


Figure 1. Typical Flash X-ray Set-Up Showing Relative Positions of the Apparatus

Mass calculations involve the equation for the volume of a truncated cone. As described in Appendix A, points located around the film image of a particle outline a pair of trapezoids. This is also shown in Figure 2. The program interprets the coordinates of the points as measurements for truncated cones and applies the equation for mass, m , where

$$m = \rho \frac{\pi}{3} [H_1(R_1^2 + R_1R_2 + R_2^2) + H_2(R_2^2 + R_2R_3 + R_3^2)] .$$

Here, ρ is the density of the shaped-charge liner material, H_1 and H_2 are the heights of the truncated cones, and R_1 , R_2 and R_3 are the radii.

Momentum (mv) and kinetic energy ($\frac{1}{2} mv^2$) are finally calculated using velocity and mass previously computed.

The virtual origin of the shaped-charge jet is found by fitting a least-squares line through the particle velocity/particle position data for each flash. Theoretically, the position of the virtual origin corresponds to a particle velocity of zero.⁴

Tabulations of the above mentioned quantities are performed and listed in the output as averages. However, for the purpose of trouble-shooting, and to gain insight into the accuracy of the average computed quantities, velocities between the flashes and masses for each flash are also listed.

⁴R. DiPersio, J. Simon and A. B. Merendino, "Penetration of Shaped-Charge Jets Into Metallic Targets," BRL Report 1296 (1965). (AD #476717).

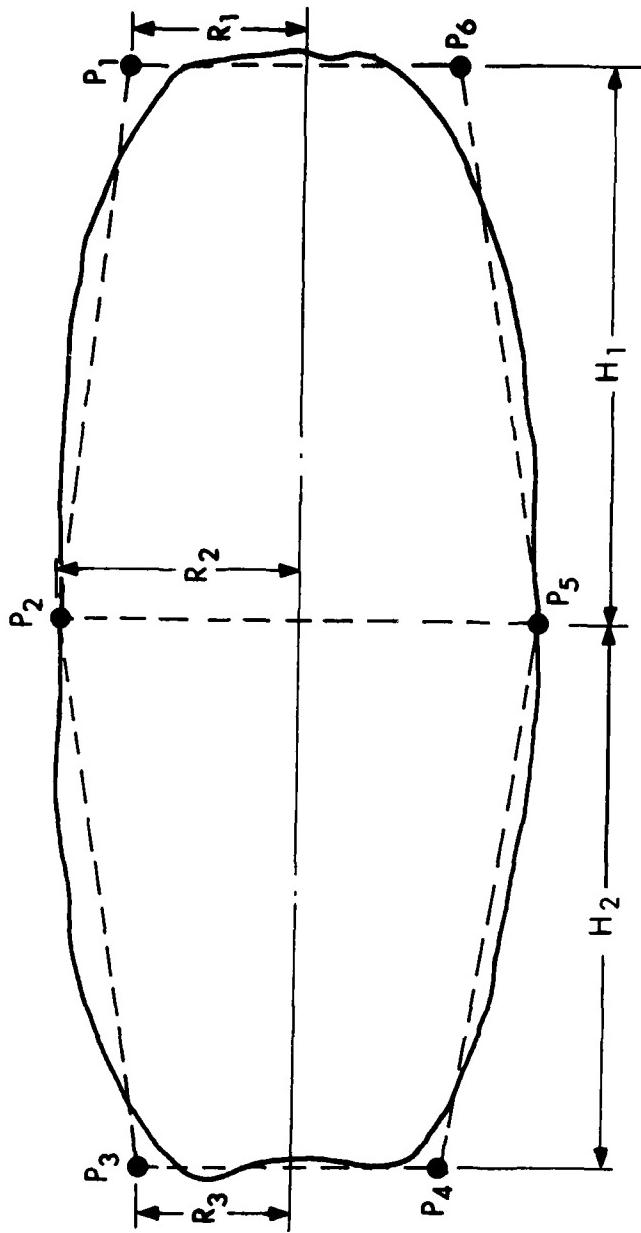


Figure 2. Particle Shape Approximation. Dashed lines outline two trapezoids that are interpreted as truncated cones in the program.

III. SUMMARY

As indicated earlier, this method quickly yields valuable information necessary for the evaluation of shaped charge designs. A large number of radiographs can be data reduced in a few days, whereas the same number would take months if reduced by hand. This has the advantage of giving the shaped charge investigator more flexibility by allowing more time to assess designs and make decisions.

For accuracy considerations, comparisons of some measurements were made with other findings, and an error estimate of one measurement was performed. Velocity, length, diameter and break-up time calculations for the round in Appendix E were compared to data of several similar rounds as reported by Majerus⁵. The quantities in Appendix E were found to be within the range of Majerus' data. There is a problem, however, with particle mass calculations. An error estimate for the mass of a selected particle revealed that the measurement could be incorrect by approximately 60%. Several factors are involved in this large error including magnification measurements, digitizing equipment accuracy, image clarity and coordinate point locations. Referring back to Figure 2, note that the group of points surrounding the particle does not represent a contour mapping of the particle shape but approximates two truncated cone geometries. This is where the largest part of the error occurs. Ideally, a much larger number of digitized points would give a better approximation of shape, but the equipment currently in use limits the number to six. One solution would be the use of a digitizer with a rapid and continuous mode point reader connected to a tape or disc data storage device. This would enable the operator to trace the image of a particle and produce a closer geometric approximation. The computer program could subsequently be modified to compute mass more accurately.

⁵J. N. Majerus, "A Model for Studying the Influence of Various Packages Upon Shaped Charge Warhead Performance," R&D Report, AD-76-1000 (1976). (AD#B015299L).

APPENDIX A
PROCEDURES FOR PREPARING AND READING RADIOGRAPHS

The standard BRL flash radiographic test site contains holders for film cassettes, each cassette containing either three or four films. As a rule the films bear the flash number and the film number.

After developing the films, they are arranged according to their positions in the cassettes. The jet particles are then numbered starting with the jet tip and working back, with each particle having the same designated number for every flash.

Once the particles are identified, a set of six points, outlining a pair of trapezoids, is obtained for each particle. When measurements are taken of these points, the configuration will be interpreted as a pair of truncated cones in order to calculate mass. Figure A-1 describes the preparation of the jet particle images.

The film reading machine that is presently used for this procedure is the Data Reducer 099, manufactured by the Telecomputing Corp. Signals are sent from the 099 to a digitizer, developed for BRL by Mr. Donald F. Merritt. The digitizer then transmitts this information, in the form of data units per inch, to a MAI Equipment Corp. 523 Gang Summary Unit which punches the data onto computer cards.

The following procedures will enable the user to operate the film reading equipment:

1. Insert the wired circuit board labeled "JET", label down, into the connection frame of the Gang Summary Unit.
2. Load the Gang Summary Unit feeder with blank computer cards.
3. Turn all three machines on, in any order.
4. Beginning with the first flash, place the film containing the jet tip onto the lighted reading surface of the 099. Arrange the film so that the jet is aligned horizontally on the lighted surface. The horizontal fiducial should run parallel to a line marked across the lighted surface as indicated in Figure 2. This is the x-direction. The vertical fiducial will indicate the y - direction.
5. By adjusting the large wheels located on either side of the console, place the cursor cross-hairs on the intersection of the x and y fiducials and press the button marked " ϕ " on the right of the console. This will assign (0,0) to the x/y intersection.
6. Located at the bottom-center of the digitizer console is a set of twelve registers with star-wheel adjustments. Reading from left to right, enter the round number in the first five registers, film number in the seventh and flash number in the eleventh.

7. The frame count windows in the center of the digitizer console should read zero in all units. If not, press the reset buttons until all units are zeroed.

8. Position the other switches and registers on the digitizer console as indicated in Table A-1.

9. With the cursor at (0,0), press the foot switch repeatedly until the number "1" appears in the frame count window. This will zero-out the memory in the card punch machine.

10. To read a particle place the cursor on each point, beginning with p_1 (Figure A-1), and press the foot switch for reading at each point. Repeat this step for every particle on the film.

Table A-1. Positions of Switches and Other Adjustments on the Electronic Digitizer

<u>SWITCH</u>	<u>POSITION</u>
Multiplier (x and y)	4
Direction (x)	Down
Direction (y)	Down
Normal/Test (x)	Normal
Normal/Test (y)	Normal
Printer (paper tape)	User's choice
Punch	on
Skip/Print Constants	Print (on)
Frame Count Advance	6

11. Repeat steps 4 through 10 for each film.

12. Change registers seven, film number, and eleven, flash number, when the film is changed.

13. After the particles are read for all flashes, sort the cards out by "reading the holes" in columns 77 through 80, and remove only the card for each particle that has punched holes for a "+" character over column 76. This will be the sixth (last) card for the particle.

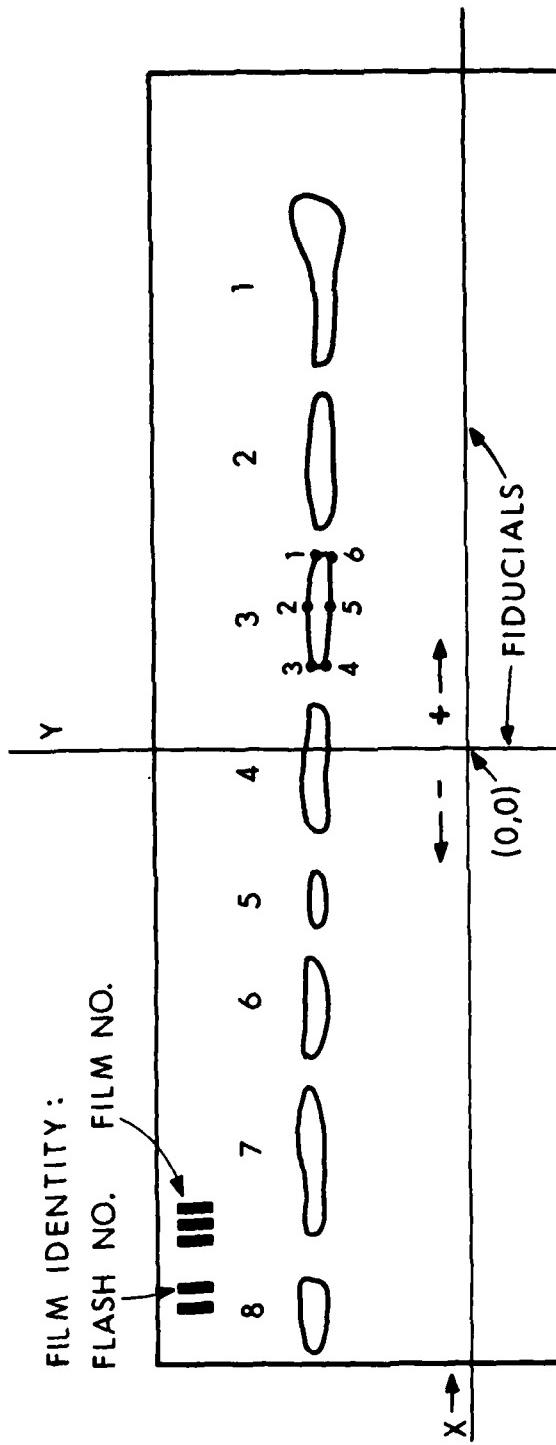


Figure A-1. Typical Radiograph of a Shaped-Charge Jet
Mounted on Film Reading Device and Showing
the Sequence for Reading a Particle

APPENDIX B
INPUT TO THE PROGRAM

Card 1:

Columns 1-5: ICASES - Number of rounds to be run.

6-10: LCL - Option for printing out the shaped-charge liner density. Enter 1 if print out is not desired. Otherwise, leave blank.

Card 2: Case Identifier and some constants.

Columns 1-5: NROUND - Round Number
6-10: NPART - Number of jet particles
11-15:NFLASH - Number of flashes
16-20: RHO - Shaped-charge liner density
21-30: XMAG1 - Magnification factor for first flash
31-40: XMAG2 - Magnification factor for second flash
41-50: XMAG3 - Magnification factor for third flash
51-60: Flash 1 - Delay time for first flash
61-70: Flash 2 - Delay time for second flash
71-80: Flash 3 - Delay time for third flash.

Card 3: More constants.

Columns 1-10: FOCUS 1 - Distance from the shaped-charge liner base to the focal level of the first x-ray tube.

11-20: FOCUS 2 - Distance from the shaped-charge liner base to the focal level of the second x-ray tube.

21-30: FOCUS 3 - Distance from the shaped-charge liner base to the focal level of the third x-ray tube.

31-40: F1A } Distances of film "y" fiducials to the

41-50: F2A } focal level of Flash A. Digit is film

51-60: F3A } number and letter (A, B or C) is flash.

61-70 F4A This also applies for Card 4 constants.

Card 4: More constants for fiducial measurements.

Columns 1-10: F1B
11-20: F2B
21-30: F3B
31-40: F4B
41-50: F1C
51-60: F2C
61-70: F3C
71-80: F4C

Card 5: First particle card. All particle cards are identical in format. x and y coordinates are data units/inch in integer form.

Columns 1-5: IX(1) - x coordinate of p₁
6-10: IY(1) - y coordinate of p₁
11-15: IX(2) - x coordinate of p₂
16-20: IY(2) - y coordinate of p₂
21-25: IX(3) - x coordinate of p₃
26-30: IY(3) - y coordinate of p₃
31-35: IX(4) - x coordinate of p₄
36-40: IY(4) - y coordinate of p₄
41-45: IX(5) - x coordinate of p₅
46-50: IY(5) - y coordinate of p₅
51-55: IX(6) - x coordinate of p₆
56-60: IY(6) - y coordinate of p₆

65: L - Flash number (1,2 or 3)
70: IFILM - Film number
71-75: IROUND - Round number
77-80: IPART - Particle number

APPENDIX C
PROGRAM LISTING

The program is written in FORTRAN IV and is currently on file
in the BRL Control Data Corporation's CYBER 170/7600 system.

```

1      PROGRAM MAIN(INPUT,OUTPUT,TAPES=INPUT,TAPEo=OUTPUT)          MAIN    2
2      DIMENSION S1(100),S2(100),S3(100),VOL(100),XL(100),DIA(100),   MAIN    3
3      LV1(100),V2(100),V3(100),VEL(100),XMASS(100),XKE(100),SUMKE(100),   MAIN    4
4      ZFLOC(100),XXL(100),SUML(100),IX(6),IY(6),ZX(4),ZY(4),   MAIN    5
5      ZMPEAK(100),SUMMAS(100),B(10000),DA(3),DR(3),XMAG(3)   MAIN    6
6      DIMENSION AA(2,3),CC(2),MR(500),AF(500),SIG(2),TT(2)   COFFMA  1
7      DIMENSION SA(10),SB(10),SC(10),SD(10),SE(10),SF(10),SL1(10)   MAIN    7
8      ISL2(10),SL3(10),ST(10),L1(100),L2(100),L3(100)   MAIN    8
9      DIMENSION P(100),TOTP(100),SUMDIA(100),SUMLEN(100),XDIA(100),DELV(   MAIN    9
10     1100),SDELV(100),SUMDEL(100)   MAIN   10
11     DIMENSION XVOL(3,100)   MAIN   11
12     DIMENSION AZ(100,100)   COPRF   1
13     DATA SA(1),SA(2),SA(3)/10HVELOCITY (.+10HMM/MICROSE+3HC)>/   MAIN   12
14     DATA SB(1),SB(2),SB(3)/10HCUMULATIVE,10H MASS (GRA.+4HMS)>/   MAIN   13
15     DATA SC(1),SC(2),SC(3),SC(4)/10HPOSITION A.+10HLONG JET L.+10HENUTH   MAIN   14
16     1(MW).1H/>   MAIN   15
17     DATA SD(1),SD(2),SD(3)/10HCUMULATIVE,10H R.E. (JOU.+5HLES)>/   MAIN   16
18     DATA SE(1),SE(2),SE(3),SE(4)/10HDISTANCE F.+10HMM CHARGE.+10H BASE   MAIN   17
19     1(MW).1H/>   MAIN   18
20     DATA SF(1),SF(2),SF(3)/10HWEAK=UP T.+10HINE (MICRC.+5HSEC)>/   MAIN   19
21     DATA SL1(1)/0HFLASH 1>/   MAIN   20
22     DATA SL2(1)/0HFLASH 2>/   MAIN   21
23     DATA SL3(1)/0HFLASH 3>/   MAIN   22
24     1 FORMAT(3IS,FS,2+6F10.5)   MAIN   23
25     2 FORMAT(7F10.5)   MAIN   24
26     6 FORMAT(8F10.5)   MAIN   25
27     21 FORMAT(2IS)   MAIN   26
28     30 FORMAT(12IS,2X,11,2X,3IS)   MAIN   27
29     HEAD(5,21) ICASES,LCL
30     IF.EOF(5)) 23,23   MAIN   28
31     23 DO 500 IJ=1,ICASES   MAIN   29
32     22 READ(5,1)NROUND,NPAHT,NFLASH,RHO,(XMAG(I),I=1+3),FLASH1,FLASH2,   MAIN   30
33     1FLASH3
34     IF.EOF(5)) 24,24   MAIN   31
35     24 ENCODE(21+20,ST(1)) NROUND   MAIN   32
36     20 FORMAT(10HROUND NUMB,+HER +15.2H >)   MAIN   33
37     HEAD(5,2) FOCUS1,FOCUS2,FOCUS3,F1A,F2A,F3A,F4A
38     IF.EOF(5)) 25,25   MAIN   34
39     25 HEAD(5,6) F1B,F2B,F3B,F4B,F1C,F2C,F3C,F4C   MAIN   35
40     IF.EOF(5)) 26,26   MAIN   36
41     26 R0=RHO   MAIN   37
42     IF(LCL,NE,1) GO TO 29   MAIN   38
43     RHO=0.   MAIN   39
44     C
45     C       ROUND INFORMATION CARD NFAT   MAIN   40
46     C       POINT S   MAIN   41
47     C       LET NT 3, NROUND+RHO,(XMAG(N),N=1+3),FOCUS1,FOCUS2,FOCUS3,FLASH1,FL   MAIN   42
48     C       14SH2,FLASH3   MAIN   43
49     C       3 FORMAT(1//,20X,ROUND NUMBER +,IS,/,20X,LINEAR DENSITY(GM/CC)-   MAIN   44
50     C       1 ,F4.1/,20X,MAGNIFICATION FACTOR-+3F9.5,/,20X,DISTANCE F'UM L   MAIN   45
51     C       21E BASE TO FOCAL POINT(MM)+,25X,FLASH 1= ,F6.1/,25A,FLASH   MAIN   46
52     C       32- ,F6.1/,25X,FLASH 3= ,F6.1/,20A,DELAY TIMES (MICROSEC)+/,   MAIN   47
53     C       425X,FLASH 1= ,F6.1/,25X,FLASH 2= ,F6.1/,25X,FLASH 3= ,F6.1   MAIN   48
54     C
55     C       RHO=0.0   MAIN   49
56     C       POINT S   MAIN   50
57     5 FORMAT(1H1)   MAIN   51

```

```

      PRINT *
  4 FORMAT(2X,'PARTICLE AVG. VELOCITY TOTAL JET BREAK-UP',/2
  12X,'NUMBER',/4X,'(MM/MICROSEC)',/3X,'LENGTH(MM)',/3X,'(MICROSEC)',/)

  60      P1=3.14159
  61      DO 150 I=1,NFLASH
  62      DO 149 J=1,NPAHT
  63      RFAD(5,30)(IX(K),IY(K),K=1,6)=L*IFILM*IROUND(IPAHT
  64      IF(EGF(S)) 32,32
  65      32 DO 35 M=1,6
  66      ZX(M)=FLOAT(IX(M))/15.4906
  67      ZY(M)=FLOAT(IY(M))/15.4906
  68      IF(ZX(1).EQ.ZX(2)) GO TO 40
  69      R1=.5*SQRT((ZX(1)-ZX(6))*2+(ZY(1)-ZY(6))*2)*XMAG(I)
  70      R2=.5*SQRT((ZX(2)-ZX(5))*2+(ZY(2)-ZY(5))*2)*XMAG(I)
  71      R3=.5*SQRT((ZX(3)-ZX(4))*2+(ZY(3)-ZY(4))*2)*XMAG(I)
  72      P1X=(ZX(1)+ZX(6))/2.
  73      P1Y=(ZY(1)+ZY(6))/2.
  74      P2X=(ZX(3)+ZX(4))/2.
  75      P2Y=(ZY(3)+ZY(4))/2.
  76      P3X=(ZX(2)+ZX(5))/2.
  77      AZ(I+J)=(ZY(2)+ZY(5))/2.
  78      P3Y=(ZY(2)+ZY(5))/2.
  79      XH1=SQRT((P1X-P3X)**2+(P1Y-P3Y)**2)*XMAG(I)
  80      XH2=SQRT((P3X-P2X)**2+(P3Y-P2Y)**2)*XMAG(I)
  81      P1Z=P1X
  82      P1X=P2X
  83      GOTO 45
  84      40 P1X=ZX(1)
  85      IF(L.EQ.2) GOTO 55
  86      IF(L.EQ.3) GOTO 65
  87      IF(IFILM.EQ.2) GO TO 67
  88      IF(IFILM.EQ.3) GO TO 68
  89      IF(IFILM.EQ.4) GO TO 69
  90      S1(J)=FOCUS1-(F1A-P1X)*XMAG(I)
  91      GO TO 15
  92      47 S1(J)=FOCUS1-(F2A-P1X)*XMAG(I)
  93      GO TO 15
  94      48 S1(J)=FOCUS1-(F3A+P1X)*XMAG(I)
  95      GO TO 15
  96      49 S1(J)=FOCUS1-(F4A+P1X)*XMAG(I)
  97      15 IF(ZX(1).EQ.ZX(2)) GO TO 50
  98      L1(J)=0
  99      GOTO 75
 100      50 L1(J)=1
 101      GOTO 40
 102      55 IF(IFILM.EQ.2) GO TO 57
 103      IF(IFILM.EQ.3) GO TO 58
 104      IF(IFILM.EQ.4) GO TO 59
 105      S2(J)=FOCUS2-(F1B-P1X)*XMAG(I)
 106      GO TO 16
 107      57 S2(J)=FOCUS2-(F2B-P1X)*XMAG(I)
 108      GO TO 16
 109      58 S2(J)=FOCUS2-(F3B+P1X)*XMAG(I)
 110      GO TO 16
 111      59 S2(J)=FOCUS2-(F4B+P1X)*XMAG(I)
 112      16 V1(J)=(S2(J)-S1(J))/(FLASH2-FLASH1)
 113      IF(ZX(1).EQ.ZX(2)) GO TO 50

```

115	L2(J)=0	MAIN	113
	GOTO 75	MAIN	114
60	L2(J)=1	MAIN	115
	GOTO 80	MAIN	116
65	IF(IFFLASH.EQ.2) GOTO 80	MAIN	117
120	IF(IFILM.EQ.2) GO TO 67	MAIN	118
	IF(IFILM.EQ.3) GO TO 68	MAIN	119
	IF(IFILM.EQ.4) GO TO 69	MAIN	120
	S3(J)=FOCUS3-(F1C-P1X)*XMAG(I)	MAIN	121
	GO TO 17	MAIN	122
125	67 S3(J)=FOCUS3-(F2C-P1X)*XMAG(I)	MAIN	123
	GO TO 17	MAIN	124
	68 S3(J)=FOCUS3-(F3C-P1X)*XMAG(I)	MAIN	125
	GO TO 17	MAIN	126
69	S3(J)=FOCUS3-(F4C-P1X)*XMAG(I)	MAIN	127
130	17 V2(J)=(S3(J)-S2(J))/(FLASH3-FLASH2)	MAIN	128
	V3(J)=(S3(J)-S1(J))/(FLASH3-FLASH1)	MAIN	129
	IF(ZX(1).EQ.ZX(2)) GO TO 70	MAIN	130
	L3(J)=0	MAIN	131
	GOTO 75	MAIN	132
135	70 L3(J)=1	MAIN	133
	GOTO 80	MAIN	134
75	VOL(J)= VOL(J)*(PI*XH1/3.*((H)**2*R1*R2*R2**2)+PI*XH2/3.*((H2**2+H2**2)*	MAIN	135
	(R1+R3**2))	MAIN	136
	PI*XH1*Z	MAIN	137
140	XVOL(I,J)= PI*XH1/3.*((R1**2+R1*R2+R2**2)+H1*XH2/3.*((H2**2+H2**2)*	MAIN	138
	(R2**2))	MAIN	139
	XVOL(I,J)= XVOL(I,J)*.001*RH0	MAIN	140
	XL(J)=XL(J)+SQR((P1X-P2X)**2+(P1Y-P2Y)**2)*XMAG(I)	MAIN	141
	DIA(J)=DIA(J)+2.*R2	MAIN	142
145	H0 CONTINUE	MAIN	143
	IF(I.LT.NFLASH) GOTO 149	MAIN	144
	IF(IFFLASH.EQ.2) GOTO 95	MAIN	145
	IF(L1(J).EQ.1.AND.L2(J).EQ.1.AND.L3(J).EQ.1) GO TO 149	MAIN	146
150	IF(L1(J).EQ.0.AND.L2(J).EQ.0.AND.L3(J).EQ.0) GO TO 90	MAIN	147
	IF(L2(J).EQ.1.AND.L3(J).EQ.1) GO TO 95	MAIN	148
	IF(L1(J).EQ.1.AND.L3(J).EQ.1) GO TO 95	MAIN	149
	IF(L1(J).EQ.0.AND.L2(J).EQ.1) GO TO 95	MAIN	150
	IF(L2(J).EQ.0.AND.L3(J).EQ.1) GO TO 100	MAIN	151
155	IF(L1(J).EQ.0.AND.L3(J).EQ.0) GO TO 100	MAIN	152
	IF(L1(J).EQ.0.AND.L2(J).EQ.0) GO TO 100	MAIN	153
160	45 IF(L1(J).EQ.1.AND.L2(J).EQ.1) GO TO 149	MAIN	154
	IF(L1(J).EQ.0.AND.L2(J).EQ.0) GO TO 100	MAIN	155
	IF(L1(J).EQ.0.0H.L2(J).EQ.0) GO TO 95	MAIN	156
165	90 XMASS(J)=VOL(J)*.001/3.*RH0	MAIN	157
	XL(J)=XL(J)/3.	MAIN	158
	DIA(J)=DIA(J)/3.	MAIN	159
	GOTO 149	MAIN	160
	45 XMASS(J)=VOL(J)*.001*RH0	MAIN	161
	GOTO 149	MAIN	162
170	130 XMASS(J)=VOL(J)*.001/2.*RH0	MAIN	163
	XL(J)=XL(J)/2.	MAIN	164
	DIA(J)=DIA(J)/2.	MAIN	165
175	149 CONTINUE	MAIN	166
	150 CONTINUE	MAIN	167
	GO 170 N=1.NPAHT	MAIN	168
	IF(IFFLASH.EQ.2) GOTO 155	MAIN	169

```

VEL(N)=V1(N)+V2(N)+V3(N))/3.0.
GOTO 160
175 VFL(N)=V1(N)*.1
160 SUML(N)=XL(N)+SUML(N-1)
SUMMAS(N)=XMASS(N)+SUMMAS(N-1)
ELOD(N)=XL(N)/DIA(N)
VEL(N)=VEL(N)*10.
XKE(N)=.5*XMASS(N)*.001*(VEL(N)*1000.)**2
SUMKE(N)=XKE(N)+SUMKE(N-1)
P(N)=VEL(N)*XMASS(N)
TOTP(N)=P(N)+TOTP(N-1)
SUMDIA(N)=SUMDIA(N-1)+DIA(N)
IF(N.EQ.1)GOTO 165
145 HREAK(N)=SUML(N)/(VEL(1)-VEL(N))
GOTO 170
165 HREAK(1)=0.0
170 PRINT 171, N,VEL(N),SUML(N),HREAK(N)
171 FORMAT(23X,I2.10X,F6.3,9X,F6.2,7X,F6.1)
172 PRINT 52
52 FORMAT(1H1,20X,'PARTICLE',4X,'VELOCITY1',4X,'VELOCITY2',4X,
1'VELOCITY3',4X,'NUMBER',3X,'(MM/MICROSEC)',2X,'(MM/MICROSEC)',1,
22X,'(MM/MICROSEC)',1,/)
DO 172 J=1,NPART
172 PRINT 173, J,V1(J),V2(J),V3(J)
173 FORMAT(23X,I2,9X,F6.3,9X,F6.3,9X,F6.3)
PRINT 175
175 FORMAT(1H1,20X,'PARTICLE LENGTH DIA. L/D MASS TOTAL J MAIN
1ET',4X,'NUMBER',5X,'(MM)',4X,'(MM)',9X,'(GRAMS)',2X,'MASS(GRAMS)'1,
2)',1)
DO 176 I=1,NPART
176 PRINT 177, I,XL(I),DIA(I),ELOD(I),AMASS(I)+SUMMAS(I)
177 FORMAT(23X,I2,6X,F4.1,4X,F4.1,2X,F4.1,4X,F5.2,5X,F4.2)
PRINT 603
205 603 FORMAT(1H1,20X,'PARTICLE',4X,'MASS1',9X,'MASS2',9X,'MASS3',4X,22X,
1'NUMBER',4X,'(GRAMS)',7X,'(GRAMS)',7X,'(GRAMS)',1,/)
DO 600 J=1,NPART
600 I=1
500 WRITE(6,602) I,J,XVOL(I+J),XVOL(I+1+J),XVOL(I+2+J)
602 FORMAT(23X,I2,6X,F8.4,6X,F8.4,6X,F8.4)
PRINT 180
180 FORMAT(1H1,20X,'PARTICLE K.E. TOTAL JET [INSTANCE FROM CM MAIN
1ARGE BASE',4X,'NUMBER',4X,'(JOULES)',3X,'*KE(JOULES)',2X,'FLASH CORPA
21',2X,'FLASH 2',2X,'FLASH 3',1,/)
DO 181 I=1,NPART
181 PRINT 182, I,XKE(I),SUMKE(I),S1(I),S2(I),S3(I)
182 FORMAT(23X,I2,7X,F8.0,4X,F8.0,4X,F5.0,4X,F5.0,4X,F5.0)
PRINT 183
183 FORMAT(1H1,20X,'PARTICLE',4X,'MOMENTUM',4X,'TOTAL JET',4X,23X,'NUMB CORPA
1ER',4X,'(KG-M/SEC)',3X,'MOMENTUM',1,/)
DO 185 I=1,NPART
185 PRINT 186,I,P(I),TOTP(I)
186 FORMAT(23X,I2,9X,F6.2,7X,F6.2)
PRINT 33
33 FORMAT(1H1,21X,'PARTICLE',4X,'DEVIANCE FROM PATH (MM)',4X,23X,
1'NUMBER',6X,'FLASH 1 FLASH 2 FLASH 3',1,/)
DO 800 JJJ=1,NPART
800 WRITE (6,36) JJJ,AZ(1,JJJ),AZ(2,JJJ),AZ(3,JJJ)

```

	36 FORMAT(24X,I2,8X,F6.3,3X,F8.3+3X,F8.3)	CORRA	H
230	400 CONTINUE	CORRA	9
	DO 192 N=2,NPART	MAIN	219
	SUMLEN(N)=SUMLEN(N-1)+XL(N)	MAIN	220
	XDIA(N)=XDIA(N-1)+DIA(N)	MAIN	221
	IF(N.EQ.2) GO TO 191	MAIN	222
	DELV(N)=VEL(N-1)-VEL(N)	MAIN	223
	GO TO 192	MAIN	224
	191 DELV(N)=VEL(1)-VEL(N)	MAIN	225
	192 SVELV(N)=SDELV(N-1)+DFLV(N)	MAIN	226
	DO 195 J=3,NPART	MAIN	227
240	195 SUMDEL(J)=DELV(J)+SUMDEL(J-1)	MAIN	228
	AVL1=SUML(NPART)/FLOAT(NPART)	MAIN	229
	AVL2=SUMLEN(NPART)/FLOAT(NPART-1)	MAIN	230
	AVD1=SUMDIA(NPART)/FLOAT(NPART)	MAIN	231
	AVD2=XDIA(NPART)/FLOAT(NPART-1)	MAIN	232
245	ADELV1=SDELV(NPART)/FLOAT(NPART-1)	MAIN	233
	ADELV2=SUMDEL(NPART)/FLOAT(NPART-2)	MAIN	234
	PRINT 200, AVL1,AVL2,AVD1,AVD2,ADELV1,ADELV2	MAIN	235
250	200 FORMAT(1H1, //, 4TX, 'WITH JET TIP', //, 2DX, 'AVERAGE PART', 1ICLE LENGTH', 7X, F6.2, 7X, F6.2, //, 2DX, 'AVERAGE PARTICLE DIAMETER', 6A, 2F5.2, 8A, F5.2, //, 2DX, 'AVERAGE CHANGE IN VELOCITY', 6X, F4.2, 9A, F4.2)	MAIN	236
	PRINT 505	MAIN	237
	NRA=2	CORRA	238
	NN=1	CORRA	24
	IC=0	CORRA	25
255	CALL POLYLS(VEL,S1,NPART,AA,NRA,NN,CC,RR,AF,ERMS,SIG,TT,DET,IC)	CORRA	26
	*WHITE(6,41) CC(1)	CORRA	27
	*1 FORMAT(20X, ' VIRTUAL ORIGIN FOR FLASH 1', F12.6)	CORRA	28
	CALL POLYLS(VEL,S2,NPART,AA,NRA,NN,CC,RR,AF,ERMS,SIG,TT,DET,IC)	CORRA	29
	*WHITE(6,42) CC(1)	CORRA	30
260	*2 FORMAT(20X, ' VIRTUAL ORIGIN FOR FLASH 2', F12.6)	CORRA	31
	IF(L.LT.3) GO TO 515	CORRA	32
	CALL POLYLS(VEL,S3,NPART,AA,NRA,NN,CC,RR,AF,ERMS,SIG,TT,DET,IC)	CORRA	33
	*WHITE(6,43) CC(1)	CORRA	34
	*3 FORMAT(20X, ' VIRTUAL ORIGIN FOR FLASH 3', F12.6)	CORRA	35
265	515 CONTINUE	CORRA	36
	505 FORMAT(1H1)	MAIN	240
	DO 510 JN= 1,NPART	MAIN	241
	VOL(JN)=0.	MAIN	242
	XL(JN)=0.	MAIN	243
270	510 DIA(JN)=0.	MAIN	244
	500 CONTINUE	MAIN	245
	STOP	MAIN	246
	END	MAIN	247

APPENDIX D
ALPHABETICAL LISTING OF PROGRAM VARIABLE NAMES

ADELV1: Average change in velocity between particles.

ADELV2: Average change in velocity between particles, excluding the jet tip.

AVD1: Average diameter of all particles.

AVD2: Average diameter of particles, excluding the jet tip.

BREAK: Break-up time.

DELVA: Change in velocity between particles.

DIA: Diameter of a particle.

ELOD: Length-to-diameter ratio of a particle.

L1, L2, L3: Flags for flashes 1,2 and 3 used for determining the average length, diameter and mass of a particle.

P: Momentum of a particle.

P1X, P2X, P3X: Computed x coordinates of points between p_1 and p_6 , p_3 and p_4 , and p_2 and p_5 , respectively.

P1Y, P2Y, P3Y: Computed y coordinates of points between p_1 and p_6 , p_3 and p_4 , and p_2 and p_5 , respectively.

R1: Radius of the front end of a particle.

R2: Radius of the mid-section of a particle.

R3: Radius of the back end of a particle.

S1: Computed distance from the shaped-charge liner base to the back end of a particle for the first flash.

S2: Computed distance from the shaped-charge liner base to the back end of a particle for the second flash.

S3: Computed distance from the shaped-charge liner base to the back end of a particle for the third flash.

SDELV: Summation of the changes in velocities between particles, used in the calculation of average change in velocity.

SUMDEL: Summation of the changes in velocities between particles excluding the jet tip.

SUMDIA: Summation of the diameters of all particles, used to compute average diameter.

SUMKE: Summation of all particle kinetic energies.

SUML: Summation of the lengths of all particles.

SUMLEN: Summation of the lengths of particles excluding the jet tip.

SUMMAS: Summation of the masses of all particles.

TOTP: Summation of the momentums of all particles.

V1: Velocity computed between the first and second flashes.

V2: Velocity computed between the second and third flashes.

V3: Velocity computed between the first and third flashes.

VEL: Average velocity of V1, V2 and V3.

VOL: Summation of the volumes of a particle over all flashes.

XDIA: Summation of all particle diameters excluding the jet tip.

XH1: Height of the truncated cone on the front end of a particle.

XH2: Height of the truncated cone on the back end of a particle.

XKE: Kinetic energy of a particle.

XL: Length of a particle averaged over all flashes.

XMASS: Mass of a particle averaged over all flashes.

XVOL: Mass of a particle for a particular flash.

ZX: X coordinate converted from data units/inch to millimeters.

ZY: Y coordinates converted from data units/inch to millimeters.

APPENDIX E
OUTPUT FROM A SAMPLE RUN

ROUND NUMBER 2203

LINER DENSITY(GM/CC)- 8.9

MAGNIFICATION FACTOR- .92000 .92000 .92000

DISTANCE FROM LINER BASE TO FOCAL POINT(MM)

FLASH 1- 914.4

FLASH 2- 914.4

FLASH 3- 914.4

DELAY TIMES (MICROSEC)

FLASH 1- 161.9

FLASH 2- 183.1

FLASH 3- 202.9

PARTICLE NUMBER	AVG. VELOCITY (MM/MICROSEC)	TOTAL JET LENGTH(MM)	BREAK-UP (MICROSEC)
1	7.741	30.93	0.0
2	7.549	42.00	214.8
3	7.476	54.87	207.1
4	7.371	77.95	210.4
5	7.123	87.68	141.4
6	7.046	97.79	140.7
7	6.918	107.25	130.3
8	6.899	110.82	131.6
9	6.863	116.90	133.2
10	6.776	131.93	136.8
11	6.625	144.04	129.0
12	6.614	149.58	132.7
13	6.501	163.09	131.4
14	6.323	178.85	126.1
15	6.291	184.00	126.4
16	6.188	188.02	121.0
17	6.163	193.36	122.4
18	6.124	201.88	124.8
19	5.951	214.24	114.7
20	5.898	226.25	122.0
21	5.772	243.74	123.0
22	5.613	262.23	123.0
23	5.432	278.11	120.3
24	5.295	288.03	117.8
25	5.247	298.54	119.7
26	5.160	310.01	120.8
27	5.075	321.11	120.4
28	4.944	331.04	118.4
29	4.842	350.73	121.0
30	4.674	368.56	120.0
31	4.588	376.67	114.4
32	4.501	394.42	121.1
33	4.414	407.47	122.0
34	4.213	430.33	122.1
35	4.084	441.84	120.4
36	4.046	454.14	122.0
37	3.872	473.40	122.1
38	3.629	494.02	120.1
39	3.556	510.84	122.0
40	3.333	538.74	122.0
41	3.177	554.78	121.6
42	3.066	574.32	122.4
43	2.822	595.34	121.1

PARTICLE NUMBER	VELOCITY1 (MM/MICROSEC)	VELOCITY2 (MM/MICROSEC)	VELOCITY3 (MM/MICROSEC)
1	7.773	7.709	7.742
2	7.573	7.525	7.550
3	7.483	7.469	7.476
4	7.586	7.150	7.376
5	7.244	6.999	7.126
6	7.163	6.926	7.049
7	7.048	6.785	6.921
8	7.009	6.786	6.901
9	6.987	6.737	6.866
10	6.886	6.664	6.779
11	6.728	6.519	6.627
12	6.580	6.649	6.613
13	6.555	6.445	6.502
14	6.370	6.275	6.324
15	6.325	6.256	6.292
16	6.239	6.135	6.189
17	6.206	6.119	6.144
18	6.178	6.068	6.125
19	6.014	5.888	5.943
20	5.950	5.846	5.900
21	5.849	5.692	5.774
22	5.699	5.524	5.615
23	5.532	5.330	5.435
24	5.362	5.226	5.257
25	5.307	5.186	5.248
26	5.227	5.108	5.170
27	5.123	5.026	5.074
28	5.020	4.867	4.944
29	5.823	3.839	4.015
30	4.797	4.548	4.677
31	4.694	4.479	4.641
32	4.621	4.378	4.503
33	4.509	4.317	4.416
34	4.330	4.043	4.216
35	4.204	3.964	4.040
36	4.175	3.915	4.049
37	3.974	3.776	3.851
38	3.787	3.468	3.623
39	3.699	3.408	3.554
40	3.457	3.205	3.334
41	3.305	3.046	3.150
42	3.253	2.876	3.071
43	2.953	2.688	2.825

PARTICLE NUMBER	LENGTH (MM)	DIA. (MM)	L/D	MASS (GRAMS)	TOTAL JET MASS (GRAMS)
1	30.9	4.8	6.4	3.70	3.70
2	11.1	2.5	4.4	.29	3.44
3	12.9	2.9	4.5	.41	4.40
4	23.1	2.8	8.3	.73	5.14
5	9.7	2.9	3.4	.30	5.44
6	10.1	2.7	3.7	.31	5.75
7	9.5	2.3	4.1	.23	4.97
8	3.6	2.0	1.8	.07	4.04
9	6.1	2.4	2.6	.14	4.18
10	15.0	2.6	5.8	.48	4.66
11	12.1	2.4	5.0	.30	6.97
12	5.5	2.5	2.2	.15	7.12
13	13.5	2.9	4.7	.42	7.54
14	15.8	2.5	6.3	.43	7.97
15	5.1	2.2	2.3	.11	4.07
16	4.0	2.1	1.9	.07	4.14
17	5.3	2.5	2.1	.13	4.28
18	4.5	2.8	3.1	.26	4.52
19	12.4	2.8	4.4	.40	5.43
20	12.0	2.3	5.3	.27	4.14
21	17.5	2.3	7.7	.42	9.61
22	18.5	2.6	7.1	.50	10.10
23	15.9	2.6	6.0	.44	10.55
24	9.9	2.8	3.5	.31	10.86
25	10.5	2.7	3.9	.31	11.17
26	11.5	2.6	4.4	.31	11.48
27	11.1	3.0	3.7	.34	11.88
28	9.9	2.9	3.5	.34	12.20
29	14.7	2.9	6.4	.66	12.87
30	17.8	2.8	6.3	.56	13.42
31	8.1	2.9	2.8	.25	13.66
32	18.3	2.6	7.0	.51	14.17
33	12.5	3.1	4.0	.47	14.64
34	22.9	2.8	8.1	.73	14.37
35	11.5	2.9	4.0	.39	14.76
36	12.3	3.2	3.9	.46	15.22
37	14.3	3.0	6.4	.78	17.00
38	20.6	3.6	5.6	.96	17.46
39	16.8	3.0	5.6	.66	18.61
40	27.4	3.5	8.0	1.49	21.11
41	16.0	3.6	4.5	.73	21.84
42	14.5	4.0	4.9	1.10	21.94
43	21.0	3.9	5.3	1.24	23.18

PARTICLE NUMBER	MASS1 (GRAMS)	MASS2 (GRAMS)	MASS3 (GRAMS)
1	3.2790	3.7919	4.0380
2	.2431	.3145	.3044
3	.3305	.5462	.3644
4	.7037	0.0000	.7587
5	.2584	.3559	.2993
6	.2835	.3017	.3442
7	.1980	.2552	.2214
8	.0553	.0600	.0804
9	.1137	.1287	.1890
10	.4704	.4470	.5257
11	.2633	.3399	.3070
12	.1232	.1771	0.0000
13	.3949	.4784	.3792
14	.4385	.4003	.4510
15	.0947	.0979	.1233
16	.0725	.0615	.0746
17	.0923	.1691	.1431
18	.2072	.3005	.2321
19	.2944	.5067	.4109
20	.2320	.3066	.2623
21	.2049	.4622	.4894
22	.4570	.4864	.5437
23	.4447	.3612	.5205
24	.3100	.3123	.3067
25	.2868	.3094	.3424
26	.3022	.3063	.3340
27	.4153	.3907	.3757
28	.3499	.3318	.2424
29	.6938	0.0000	.6331
30	.6149	.5427	.4427
31	.3094	.1883	.2465
32	.7043	.3562	.4584
33	.4304	.5044	0.0000
34	.7279	.6434	.6305
35	.3945	.3630	.4035
36	.4736	.5001	.3942
37	.9466	.6912	.7131
38	1.2210	.9140	.7421
39	.5911	.4527	.9200
40	1.6889	1.5623	1.1957
41	.7484	.6758	.7803
42	1.2289	1.1217	.9580
43	1.3572	1.1849	1.1808

PARTICLE NUMBER	K.E. (JOULES)	TOTAL JET KE(JOULES)	DISTANCE FROM CHARGE BASE (MM)		
			FLASH 1	FLASH 2	FLASH 3
1	110950.	110950.	1005.	1170.	1323.
2	8188.	119138.	980.	1140.	1249.
3	11561.	130699.	964.	1123.	1271.
4	19862.	150560.	930.	1091.	1233.
5	7726.	158286.	915.	1069.	1217.
6	7690.	165976.	902.	1054.	1191.
7	5384.	171360.	888.	1038.	1172.
8	1552.	172912.	884.	1032.	1167.
9	3387.	176299.	876.	1025.	1158.
10	11045.	187345.	859.	1005.	1137.
11	6657.	194002.	841.	983.	1112.
12	3245.	197286.	831.	970.	1102.
13	8821.	206108.	816.	955.	1083.
14	8594.	214702.	794.	924.	1043.
15	2083.	216785.	788.	922.	1046.
16	1331.	218117.	782.	914.	1036.
17	2560.	220677.	776.	907.	1025.
18	4624.	225300.	766.	897.	1017.
19	7154.	232455.	749.	874.	963.
20	4644.	237099.	736.	862.	978.
21	6924.	244023.	715.	839.	942.
22	7807.	251830.	699.	810.	920.
23	6524.	258354.	684.	784.	842.
24	4341.	262695.	655.	762.	872.
25	4309.	267004.	645.	757.	860.
26	4196.	271200.	633.	743.	845.
27	5073.	276273.	621.	734.	829.
28	3969.	280242.	608.	714.	811.
29	7777.	288020.	587.	711.	782.
30	6009.	294024.	566.	688.	748.
31	2611.	296640.	557.	667.	746.
32	5145.	301784.	538.	634.	723.
33	4554.	306338.	523.	614.	714.
34	6515.	312853.	500.	595.	673.
35	3234.	316087.	488.	577.	645.
36	3733.	319820.	475.	562.	641.
37	5495.	325715.	452.	537.	611.
38	6315.	332030.	425.	504.	574.
39	4141.	336172.	409.	487.	555.
40	4287.	344454.	381.	464.	518.
41	3709.	348167.	366.	434.	498.
42	5182.	353344.	344.	414.	471.
43	4942.	358292.	323.	394.	434.

PARTICLE NUMBER	MOMENTUM (KG-M/SEC)	TOTAL JET MOMENTUM
1	28.67	28.67
2	2.17	30.83
3	3.09	33.93
4	5.39	39.32
5	2.17	41.49
6	2.18	43.67
7	1.56	45.23
8	.45	45.68
9	.99	46.66
10	3.26	49.92
11	2.01	51.93
12	.99	52.92
13	2.71	55.64
14	2.72	58.36
15	.66	59.02
16	.43	59.45
17	.83	60.28
18	1.51	61.74
19	2.40	64.10
20	1.57	65.77
21	2.40	68.17
22	2.78	70.45
23	2.40	73.35
24	1.64	74.49
25	1.64	76.64
26	1.62	78.26
27	2.00	80.26
28	1.61	81.86
29	3.21	85.08
30	2.57	87.65
31	1.14	88.74
32	2.29	91.07
33	2.06	93.13
34	3.04	96.23
35	1.58	97.81
36	1.84	99.65
37	3.04	102.69
38	3.48	106.17
39	2.33	108.50
40	4.97	113.48
41	2.33	115.81
42	3.38	114.14
43	3.50	122.64

	WITH JET TIP	W/O TIP
AVERAGE PARTICLE LENGTH (mm)	13.85	13.44
AVERAGE PARTICLE DIAMETER (mm)	2.84	2.74
AVERAGE CHANGE IN VELOCITY (mm/ μ sec) • 12		.17

VIRTUAL ORIGIN FOR FLASH 1= -85.114956 MM
VIRTUAL ORIGIN FOR FLASH 2= -81.133748 MM
VIRTUAL ORIGIN FOR FLASH 3= -85.896955 MM

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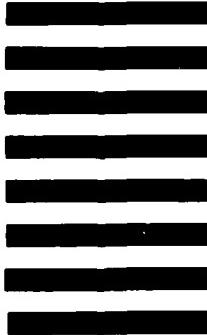


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